

Waves propagation as a tool to ranking structural quality of *Eucalyptus globulus* Labill. beams

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Eucalyptus globulus Labill.

- *Eucalyptus globulus*, cover around 700.000 ha in Spain located in Galicia, Asturias, Cantabria and Huelva.
- Although the current main use is to obtain pulp and fiber boards, its mechanical properties provide great potential for structural applications.
- Spanish standard visual grading assigned Strength grade D40 (EN1912) for small dimensions



Context

- Timber for structural applications requires grading
- Strength, stiffness and density properties need to be known for the structures design.
- Methods for the strength grading of the timber are necessary to be associated with the Visual grading
 - based on bending principle or other principles such as ultrasound, vibration, radiation, or combination of these principles

Context

- There are a lot of techniques and equipments proposed to be applied with this objective (grading) and it is important to know if the results are equivalent or correlated.

Objective

To compare the results of different nondestructive equipments, based on the wave propagation, as a tool to ranking structural quality of *Eucalyptus globulus* Labill. beams .

Material

The tests were performed on 50 beams in green conditions (68% moisture content) with 100 mm width, 150 mm high and 3000 mm length. The tests were performed in in green conditions.

**three
longitudinal
points on
transversal
sections for
each beam**



Grading tools

– Ultrasound

- Sylvatest (CBT, Swiss)
- USLab (AGRICEF, Brazil)

– Stress wave

- Microsecond Timer (Fakopp, Hungary)
- Electronic-Hammer (Instrument Mechanic Labor GmbH, German)

– Resonance

- HM200 (Fibre-Gen, New Zealand).

Ultrasound tools



Sylvatest (CBT, Swiss)

USLab (AGRICEF, Brazil)



Stress wave tools

**Electronic-Hammer (Instrumenta
Mechanic Labor GmbH, German)**



**Microsecond Timer
(Fakopp, Hungary)**



Resonance tool

HM200 (Fibre-Gen, New Zealand).



Bending test



Non destructive bending test



Destructive bending test

50 beams

MOE

5 beams (representing velocity variability)

MOR

Summary Statistics Velocities

	<i>Average m.s⁻¹</i>	<i>CV %</i>	<i>Minimum m.s⁻¹</i>	<i>Maximum m.s⁻¹</i>	<i>skewness</i>	<i>kurtosis</i>
HM 200	3558	6,18	3020	3950	-1,31	-0,53
USLAB	3858	6,01	3268	4267	-1,48	-0,33
SYLVATEST	3939	5,96	3273	4369	-1,34	0,23
IML	3671	6,68	2977	4146	-1,60	0,58
FAKOPP	3888	5,15	3264	4262	-1,38	1,36

Summary Statistics

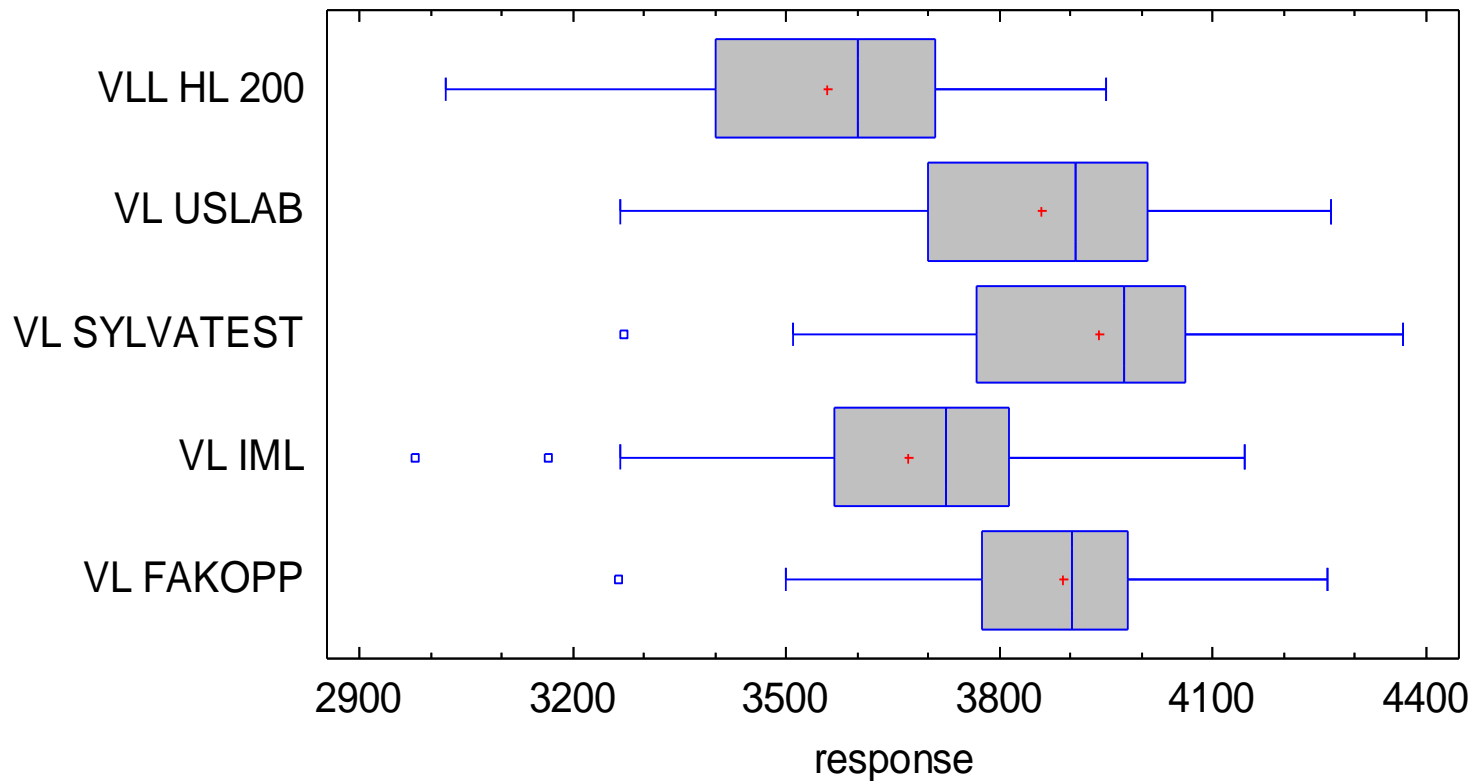
MOE and Green Density

MOE (MPa)	
Average	13022
CV (%)	11.9
Minimum	7990
Maximum	15780
Std. skewness	-2,33
Std. kurtosis	1,98

Green density (kg.m ⁻³)	
Average	1093
CV (%)	6.73
Minimum	926
Maximum	1226
Std. skewness	-0,05
Std. kurtosis	-1,08

Velocities in different tools

Box-and-Whisker Plot



Velocity comparison

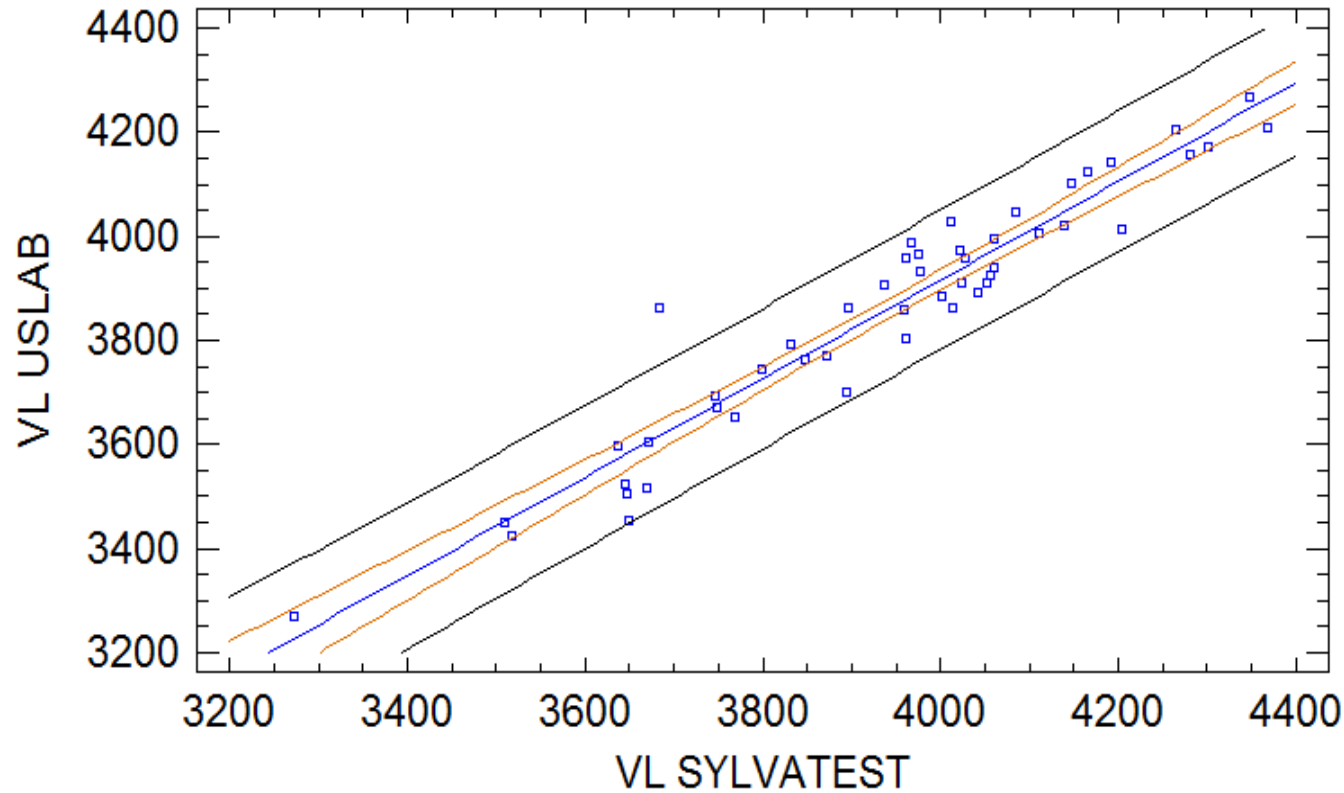
Tool	<i>Mean</i>	<i>Homogeneous Groups</i>
HM 200	3558	X
IML	3671	X
USLAB	3858	X
FAKOPP	3888	X
SYLVATEST	3939	X

Velocity Correlations

$$VL\ USLAB = 126,7 + 0,95 * VL\ SYLVATEST$$

$$R = 0,96$$

$$R^2 = 92\%$$

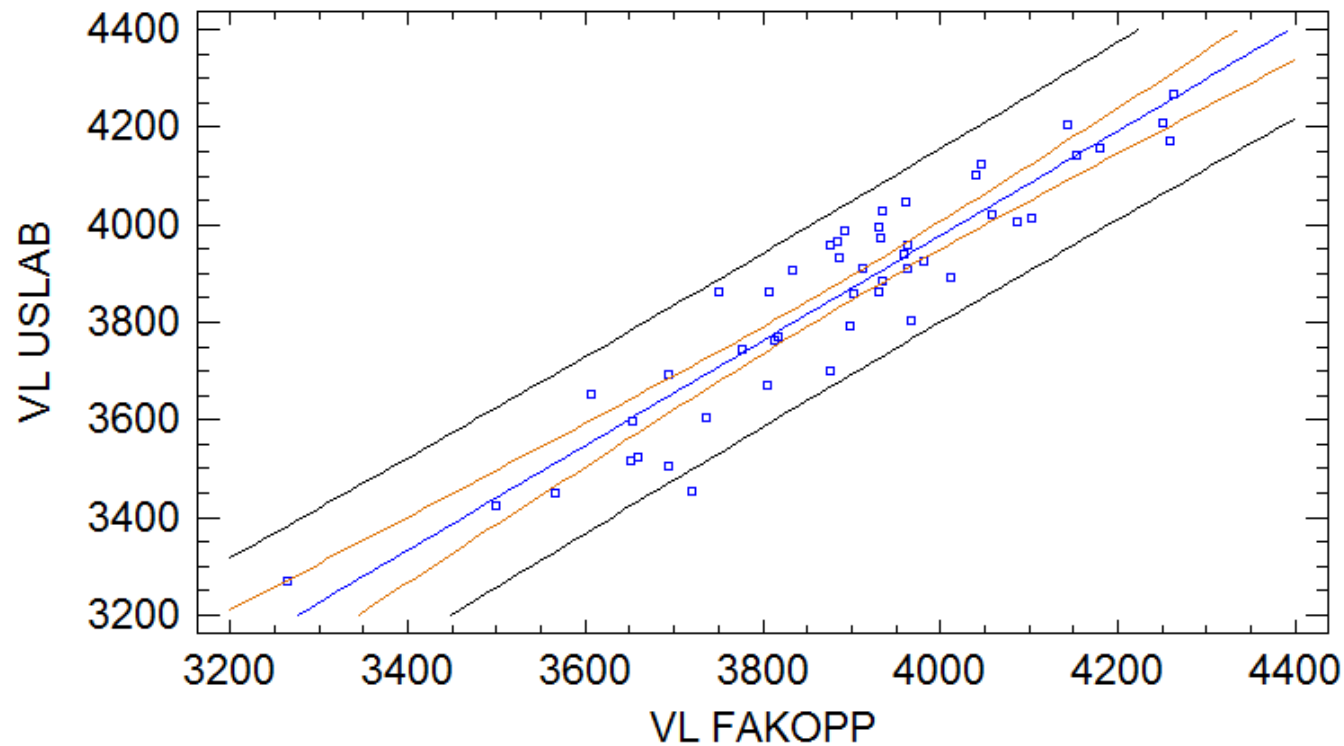


Velocity Correlations

$$VL\ USLAB = -320,1 + 1,07 * VL\ FAKOPP$$

$$R = 0,93$$

$$R^2 = 86\%$$

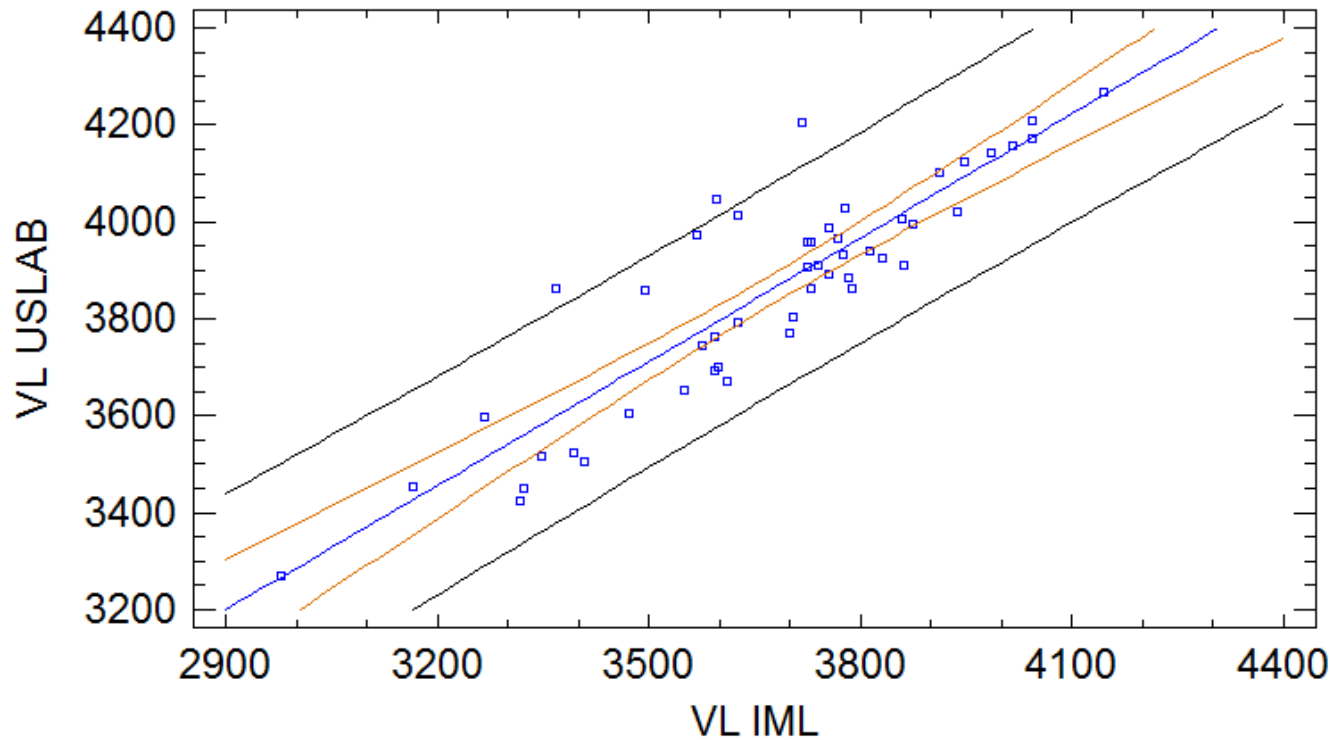


Velocity Correlations

$$VL\ USLAB = 727 + 0,85 * VL\ IML$$

$$R = 0.89$$

$$R^2 = 79\%$$

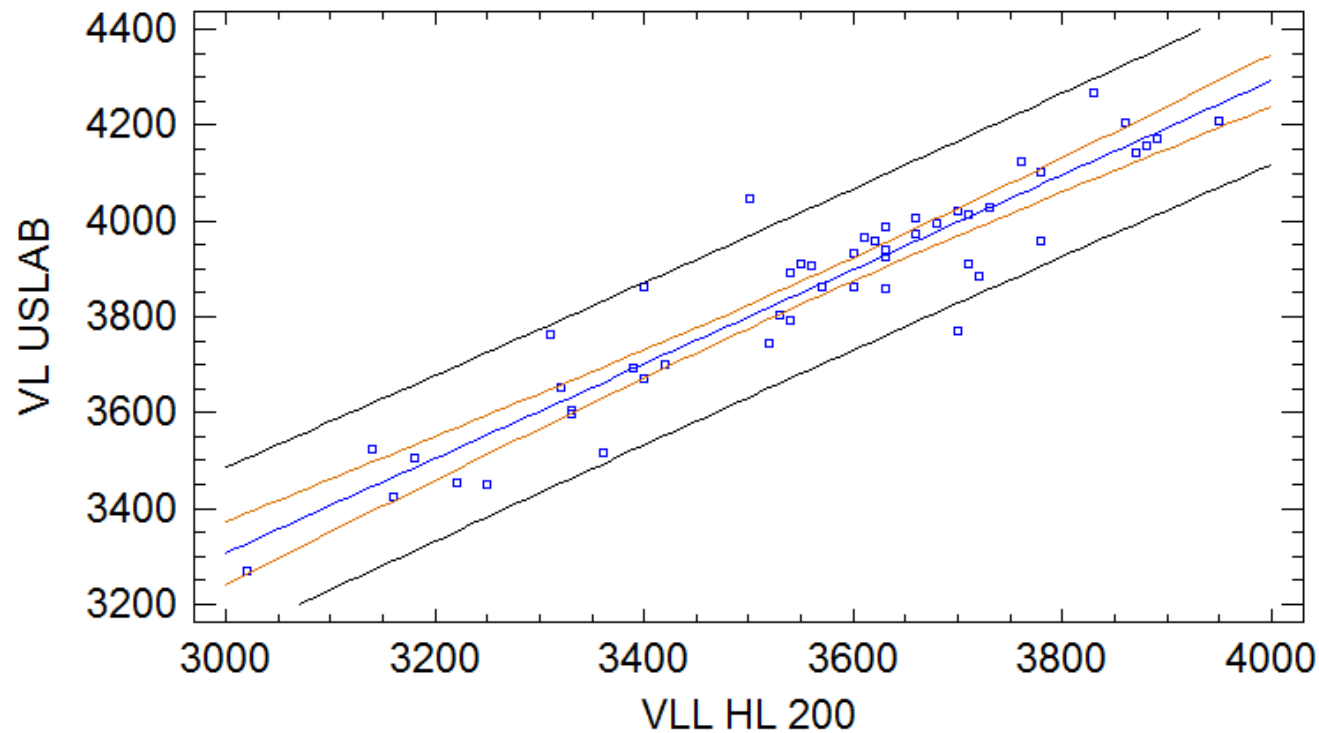


Velocity Correlations

$$VL \text{ USLAB} = 346 + 0,99 \cdot VLL \text{ HL } 200$$

$$R = 0,94$$

$$R^2 = 87\%$$



Prediction of the MOE from the velocity

Device	Model	P-Value	R	R ² (%)	Standard error
USLab (2 ⁺)	MoE static = -8113+ 4,74*Vel USLab	0,000	0,80	65,1	945
Sylvatest (2 ⁺)	MoE static = -9204,73 + 5,62*Vel Sylvatest	0,000	0,84	70,9	862
HM200 (2 ⁺)	MoE static = -7871+ 5,84*Vel Hitman	0,000	0,82	67,2	915
IML (2 ⁺)	MoE static = -5219 + 4,94*Vel IML	0,000	0,76	58,1	1035
Fakopp (2 ⁺)	MoE static = -13021 +6,6*Vel Fakopp	0,000	0,85	72,7	834

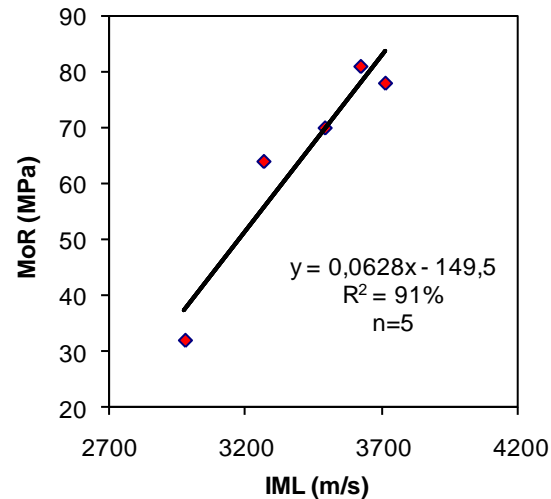
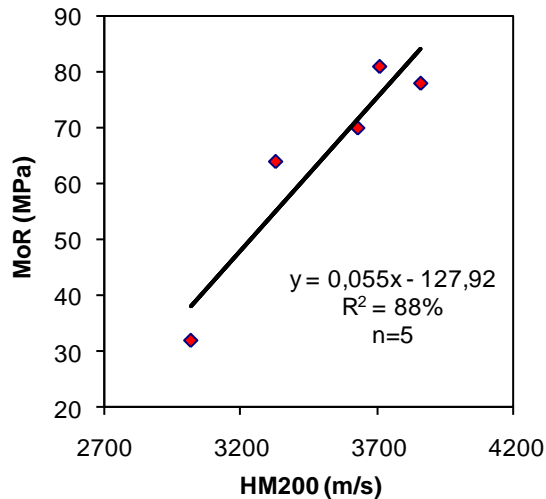
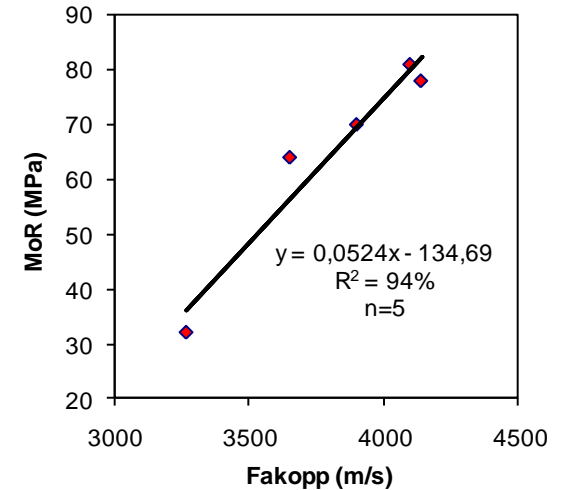
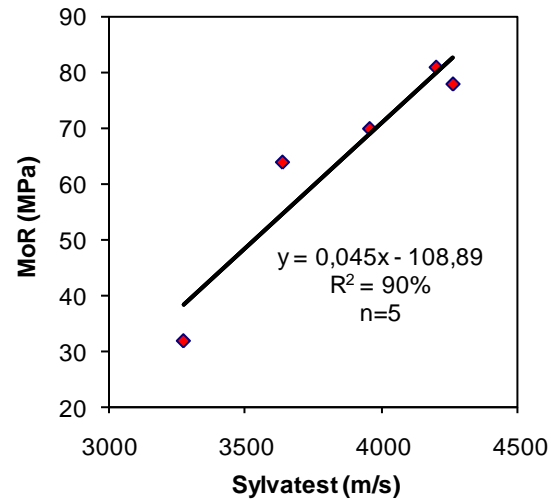
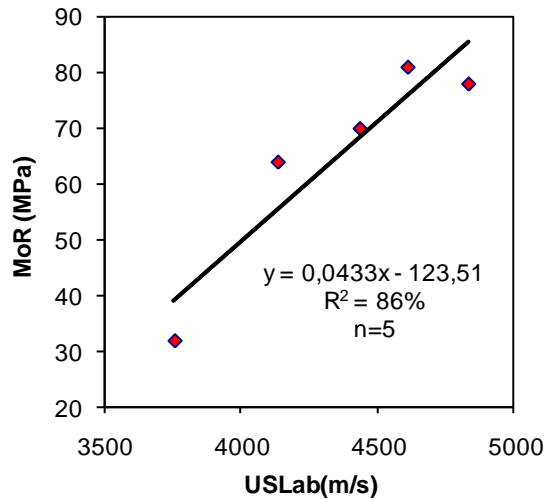
Comparison of stiffness coefficient ($CLL = \rho V^2$) and static MOE

	MOE	CLL USLAB	CLL Sylvatest	CLL HM200	CLL IML	CLL Fakopp
Average MPa	12955	16286	16979	13863	14893	16542
CV (%)	12,9	11,8	12,2	12,1	13,3	11,6
Difference (%)	-	25,7	31,1	7,0	15,0	27,7

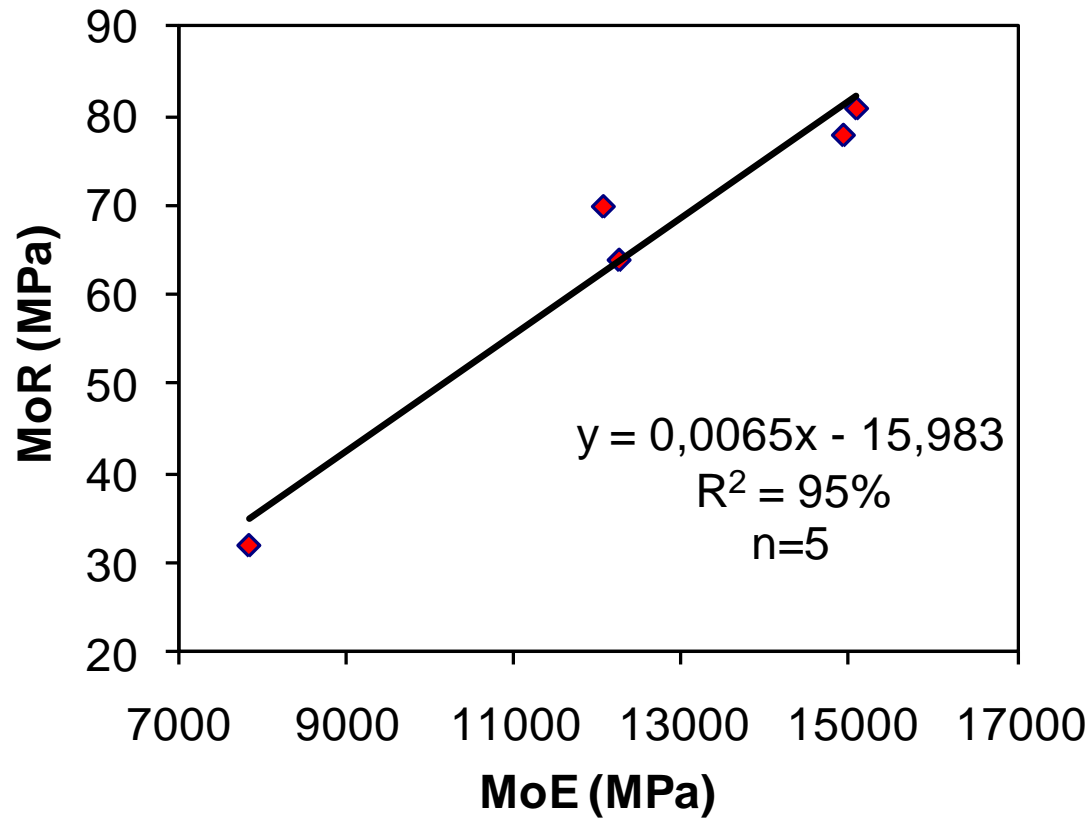
Prediction of the MOE from the CLL (stiffness coefficient)

Device	Model	P-Value	R	R ² (%)	Standard error of estimation
USLab (2) ⁺	MoE static = 1724 + 0,51*CLL	0,000	0,85	72,9	636
Sylvatest (2) ⁺	MoE static = 2209 + 0,62*CLL	0,000	0,84	71,1	778
HM200 (2) ⁺	MoE static = 1776 + 0,80*CLL	0,000	0,87	75,7	607
IML (2) ⁺⁺	MoE static = 3245 + 0,64*CLL	0,000	0,83	68,5	890
Fakopp -1	MoE static = 2639 + 0,61*CLL	0,000	0,77	60,4	998
Density (1) ^{***}	MoE static = 9350+2,73*Density	0,339 (ns)	0,14	2,1	1325

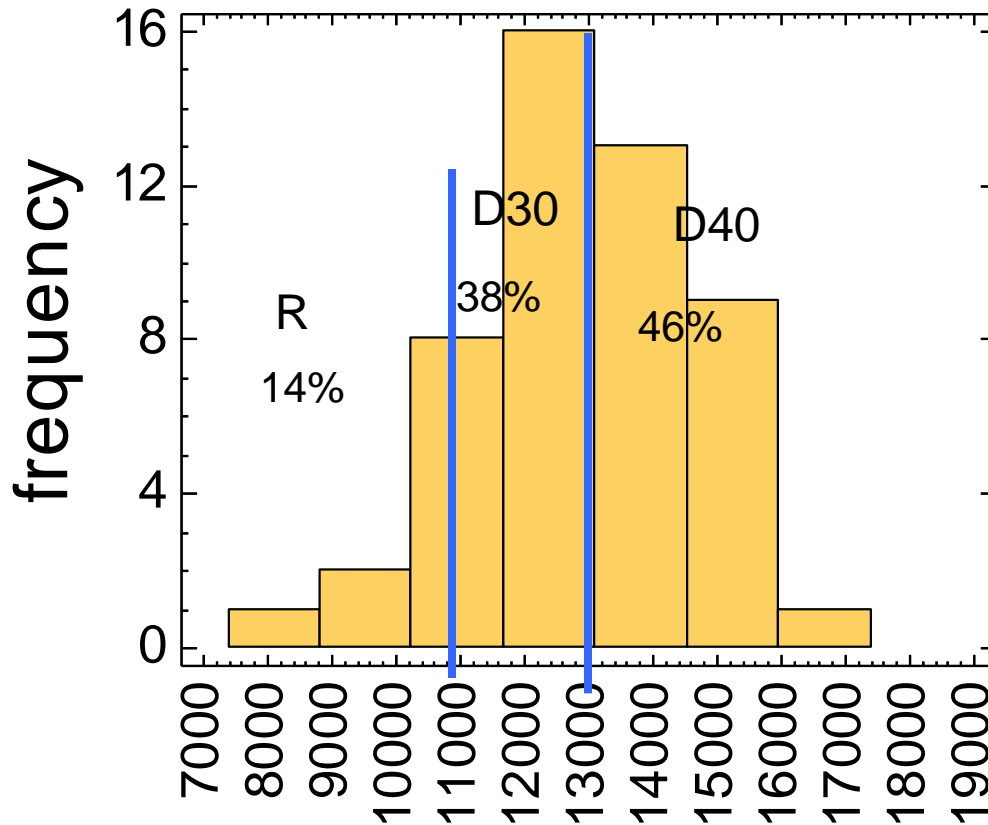
Correlation between MOR and wave velocity



Correlation between Stiffness and Strength



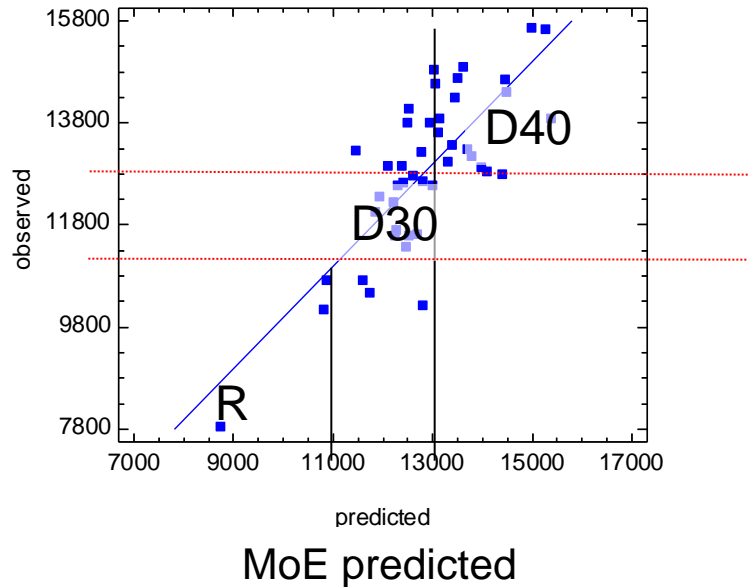
Potential strength class eucalyptus large section, according stiffness



Strength grade according Stiffness to EN 338 and considering strenght > 30 N/m²

Two potential strength class will be proposed

Acoustic grading accuracy



	USLab			Sylvatest			HM200			IML			Fakopp		
	R	D 30	D 40	R	D 30	D 40	R	D 30	D 40	R	D 30	D 40	R	D 30	D 40
Total	3	25	19	2	24	21	4	24	19	3	22	22	4	27	19
Ungraded	0	8 32%	0	0	6 25%	-	0	7 29%	-	2 66%	5 23%	-	1 25%	9 33%	-
Upgraded	-	3 12%	5 26%	0	4 16%	5 24%	-	2 8%	4 21%	-	5 23%	5 23%	-	3 11%	4 21%



Conclusions

- The velocities obtained with each tool are, in some cases, significantly different but they are all highly correlated.
- The predictive power of the modulus of elasticity with different sonic method is high and similar in all tools.
- The prediction model are, in general, better using the stiffness coefficient.

Thanks you!

